

# Low Salinity Waterflooding; A Promising Prospect to Improve Oil Recovery in the Niger Delta Oil Fields

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Received 15 October 2018; accepted 8 February 2019 Published online 22 April 2019

### Abstract

Low salinity waterflooding is considered one of the most promising and cost-effective methods in oil recovery as a result of wettability change from oil-wet to waterwet. This work considered reducing the residual oil saturation by injection of low salt concentration in order to improve oil recovery. The objective of the study is to reduce the residual oil saturation. In this study, Simulation has been carried out on a synthetic model by using (ECLIPSE 100) as the simulator. Different Salinities of 500ppm, 1000ppm, 1500ppm, 2000ppm, 5000ppm, 7000ppm, 10000ppm, 30000ppm and 40000ppm were evaluated. Low salinity water was injected at the first year of production and continues to the end of the production life.Effect of salinity on oil recovery was also evaluated. The results obtained showed that low salinity waterflooding improved oil recovery at different salinity as compared to fresh water waterflooding. In conclusion, based on the results of this work, it is possible to choose the best salinity ratio that gives the lowest residual oil saturation.

**Key words:** Low Salinity; Waterflooding; Residual oil saturation; Wettability change; Ion exchange; Mobility control

Ihekoronye, K. K., Izuwa, N. C., & Obah, B. O. (2019). Low Salinity Waterflooding; A Promising Prospect to Improve Oil Recovery in the Niger Delta Oil Fields. *Advances in Petroleum Exploration and Development*, *17*(1), 53-70. Available from: http://www.cscanada.net/index.php/aped/article/view/11005 DOI: http://dx.doi.org/10.3968/11005

# INTRODUCTION

The energy demand is increasing but discovery of huge reservoirs is scarce. The only solution to meet the energy demand is to maximize recovery from existing reservoirs. Low salinity waterflooding is an emerging EOR technique in which the salinity of the injected water is controlled to improve oil recovery. This EOR technique has recently found utility in oil industry to recover by-passed oil. Low salinity waterflooding has improved recovery through wettability alteration, reduction in interfacial tension, ionic exchange and mobilization of clay fines. The major concern will be to determine the appropriate injection scheme that will yield the best recovery. Corefloods and single-well chemical tracer tests have shown that the low salinity water flooding can improve basic water flooding recovery by about 5 to 38%.(Jerauld et al 2008)

Low salinity waterflooding (LSW) deals with several mechanism which involves the flooding of low saline water. Some techniques used to improve oil recovery in low salinity waterflooding alters the wettability of the rock (Lighthelmetal 2009)while other incorporate the concept of fine migration(Morrow etal 1998) and ion- exchange methods (Larger etal 2006). In this work, we want to establish a correlation between the salinity and oil recovery using a dimensionless number. Based on this expected result, it will be possible to determine the lowest possible low salinity adequate to recover the remaining oil. The study will also set limits on the concentration of salt required.

# 1. METHODOLOGY

In this study, we conducted numerical evaluation of low salinity waterflooding using these materials Well and reservoir data, and Eclipse Simulator used to generate field oil recovery, field oil production total, field pressure and field water cut. Table 1 shows the summary of the data used.

#### **1.1 Reservoir Model Description**

A Black oil model was designed using a centre blocked linear model geometry. The reservoir model was constructed to have grid block size of  $20 \times 20 \times 10$ . Each

grid cell is  $250 \times 250 \times 50$  (feet). The reservoirs have an area of 574 acre and made up of 4000 grids as shown in Figure 1.Thereservoir is assumed to be homogenous with respect to permeability and porosity. The simplistic reservoir model used in the simulation was built using the rock and fluid data obtained from reservoir Y-Field in the Niger Delta given in Table 1.



Figure 1 Reservoir model showinggrids

#### Table 1

Summary of the Reservoir Rock and Fluid Properties for Y-Field in the Niger Delta

Model parameter	Range
Depth (ft)	6400
Initial pressure (psi)	3288
Reservoir temperature, T (°F)	162
Oil density, (lb/ft <sup>3</sup> )	51
Water density, (lb/ft <sup>3</sup> )	62
NTG	0.89
Porosity, Φ	0.25
Permeability, k	1000md
WOC depth (ft)	6683
Water saturation, swi	0.18
API	35°
Salinity	500 ppm-40000ppm

#### Table 3 Oil and Water PVT

### **1.2 Well Description**

Four vertical oil producers (P1, P2, P3, and P4) were completed at the flange end of the oil zone for maximum reservoir contact. One water injector was drilled through the reservoir into the free water zone to maintain pressure, enhance sweep and displacement of the remaining oil.



Reservoir grid block and well connections

# 1.3 Aquifer Model

The aquifer was designed using a Carter Tracy aquifer model. This was attached to the designed reservoir model to enable fluid injection. The properties of the aquifer zone are shown in Table 2.

#### Table 2 Carter-Tracy Aquifer

		1.			
1		Initial pres- sure (psia)		Porosity	Total com- pressibility
1	6400	3288	1000	0.25	3E-6

#### 1.4 PVT Model

The PVT model was defined in the reservoir simulation. When the BRINE keyword is activated in the RUNSPEC, PVTWSALT is used to supply the water PVT data for simulation. The keyword PVTDO is used to supply the dead oil PVT data.

PR(psia)	SALT CONC (%wt)	B <sub>w</sub> (rb/stb)	B <sub>o</sub> (rb/stb)	U <sub>w</sub> (cp)	U <sub>o</sub> (cp)	Wcompressibility	API
3288	500ppm	1.02	1.121	0.3	0.55	3E-6	35
3288	1000ppm	1.02	1.121	0.3	0.55	3E-6	35
3288	1500ppm	1.02	1.121	0.3	0.55	3E-6	35
3288	2000ppm	1.02	1.121	0.3	0.55	3E-6	35
3288	5000ppm	1.02	1.121	0.3	0.55	3E-6	35
3288	7000ppm	1.02	1.121	0.3	0.55	3E-6	35
3288	10000ppm	1.02	1.121	0.3	0.55	3E-6	35
3288	30000ppm	1.02	1.121	0.3	0.55	3E-6	35
3288	40000ppm	1.02	1.121	0.3	0.55	3E-6	35

#### **1.5 Initialization Sections**

On initializing the model in Eclipse, approximately 220, 000,000 rbof oil in place was obtained for this reservoir. The wells were connected to the reservoir. Injection water of different salinity was used to study the effect of salinity on oil recovery. During the study, different ratios of injection water salinity were used. These are shown in the several case studies in this work. Table 4, 5 and 6 shows the constraints used to control the simulation in the 3 cases.

#### **1.6 Water and Oil Saturation Function**

Relative permeability for water and oil, are also defined in the reservoir simulation as shown below in Figure 3.



Figure 3 Water/oil saturation function

#### 1.7 Parameter Considered for Analysis

#### 1.7.1 Fractional flow

This is the ratio of the water flow rate to the total rate (oil and water) .These flow rate are derived from Darcy's law. The overall fractional flow of water for water-oil system is then obtained by Buckley-Leverett analysis/method shown in eqn (iv) or (v).

$$fw = \underline{qw}_{qw + qo}$$
....eqn i

$$fw = \frac{1}{1 + \frac{K_{roU_W}}{U_{O K_{rw}}}} = \frac{1}{1 + 1/M}$$
eqn ii

where fw = fraction of water in the flowing stream, bbl/ bbl

qt = total flow rate, bbl/dayqw = water flow rate, bbl/dayqo = oil flow rate, bbl/day

Eqn i-ii is used for calculation of fractional flow of water for water-oil system which was done by Buckley-Leverett method. Sw, *kro* and *krw* are taken from PROPS section under keyword SWFN.

$$S_{wd} = \frac{\text{Sw} - \text{Siw}}{1 - \text{Sor-Siw}}$$
.....eqn iii

Kro = 
$$\dot{q}_1 (1 - S_{wd})^m$$
 .....eqn iv

$$Krw = \dot{q}_2 Swd^{n} \dots eqn v$$

$$\dot{\alpha}_{1=}0.8$$
,  $\dot{\alpha}_{2}=0.2$ , m=2, n=2



Figure 4 Fractional flow (fw) verses water saturation (sw)



#### Figure 5

A plot of fractional flow (fw) against water saturation (sw)

#### ii. Sweep efficiency

 $U_o$ = 35cp,  $U_w$ = 0.4 cp,  $S_{wi}$ = 0.18,  $S_{oi}$ =1-0.18=0.82 Total primary recovery = 16.5% Sorp = 0.82-0.165 = 0.655 Total waterflood recovery = 42% = 0.42 × Sorp (0.655) = 0.2751 Sorwf = 0.655-0.2751 = 0.3799 = 0.38

# Table 4Showing Sweep Efficiencies for Different Low andHigh Salinity

Case	Scenario	Recovery efficiency (%)	Total Recovery efficiency
1	Natural depletion (0-12 years)	16.5%	0.655
2	Waterflooding (fresh water) (0-43 years)	42%	0.42 x 0.38=0.159
3	Low salinity water (500ppm) (0-46 years)	52%	0.52 x 0.38=0.198
4	Low salinity water (1000ppm) (0-46 years)	52%	0.52 x 0.38=0.198
			To be continued

#### Continued

Case		Recovery efficiency (%)	Total Recovery efficiency
5	Low salinity water (1500ppm) (0-46 years)	52%	$0.52 \times 0.38 = 0.198$
6	Low salinity water (2000ppm) (0-46 years)	52%	$0.52 \ge 0.38 = 0.198$
7	Low salinity water (5000ppm) (0-46 years)	49%	$0.49 \ge 0.38 = 0.186$
8	Low salinity water (7000ppm) (0-46 years)	49%	$0.49 \ge 0.38 = 0.186$
9	Low salinity water (10000ppm) (0-46 years)	48%	$0.48 \ge 0.38 = 0.182$
10	High salinity water (30000ppm) (0-46 years)	48%	0.48 x 0.38=0.182
11	High salinity water (40000ppm) (0-46 years	46%	0.46 x 0.38=0.175

#### **1.8 Reservoir Simulation**

The Simulation was ran and evaluated for the following cases.

Case 1: performance simulation conducted for natural depletion

Case 2: Performance simulation conducted for fresh waterflooding

Case 3:Performance simulation conducted for difference low and high salinities.

#### 1.8.1 Natural Depletion

This is the production of oil from the reservoir using the reservoir primary energy.

#### Table 5

#### Model constraint for natural depletion

Liquid production rate	4000stb/day
Maximum allowable BS & W	70%
vertical producer wells	4
Minimum BHP of the producer	1500psia

#### 1.8.2 Fresh Waterwaterflooding

This is the production of oil from the reservoir using the secondary recovery mechanism to maintain reservoir pressure and enhance reservoir sweep.

Table 6

#### Model Constraint for Waterflooding

Maximum liquid production rate	3000stb/day
Maximum allowable BS &W	80%
No of vertical producer wells	4
No of vertical injector wells	1
Minimum BHP of injector	3500psia
Surface rate	13000 stb/day

#### 1.8.3 Low Salinity Water Model

In this work, low salinity waterflooding injection was used to increase oil recovery; the salt is modeled as a single component in water phase. The option is activated by the keyword BRINE in the RUNSPEC section. Several mechanisms are involved in the displacement of oil by injection of low salinity water during production. This work allowed these mechanisms to play out during the injection. The mechanisms of low saline water (wettability change, fine migration and ion exchange) contributed to improved oil recovery in this study. The injection of low salinity water started from the first day of production and continues to the end of the production life.

# Table 7 Model Constraint for Low Salinity Water

1
4
3500 psia
13000stb/day

# 2. RESULT

#### 2.1 Result Presentation

The results of low salinity waterflood simulation are shown in Figures 4 to 25 while Table 7 displays therecovery factor, oil production, water cut and time before water production. The results are presented based on the case studies.

#### 2.1.1 Production Forecast for Natural Depletion



#### Figure 6

Plot of recovery factor and cumulative oil production total against time for natural depletion



Plot of field water cut, pressure and production rate against time for natural depletion

#### 2.1.2 Production Forecast for Waterflooding (fresh water)

The base case (*BC*) is the case of water flooding with fresh water. This flooding technique was evaluated to determine the recovery factor (FOE), field water cut (FWCT), field pressure (FPR), oil production rate (FOPR) and cumulative production total (FOPT).



Plot of recovery factor and cumulative oil production total against time for waterflooding with fresh water



Figure 9 Plot of field water cut, pressure and production rate against time for waterflooding with fresh water

2.1.3 Production Forecast for Low Salinity Water (500ppm)









### 2.1.4 Production Forecast For Low Salinity Water (1000ppm)



Plot of recovery factor and cumulative oil production total against time for Low salinity water(1000ppm)

### 2.1.5 Production Forecast for Low Salinity Water (1500ppm)













3.1.6 Production forecast for Low Salinity Water (2000ppm)













Plot of field water cut, pressure and production rate against time for low salinity water (5000 ppm)









### 3.1.9 Production Forecast for Low Salinity Water (10000ppm)







Figure 21 Plot of field water cut, pressure and production rate against time for low salinity waterflooding (7000ppm)



# Figure 23 Plot of field water cut, pressure and production rate against time for low salinity waterflooding (10000 ppm)

#### 3.1.10 Production Forecast for High Salinity Water (30000ppm)

High salinity (HS) with salt concentration 30,000 ppm is used as formation water. In this study, we assumed formation water has salinity equal to sea water that is 30000 ppm.



Figure 24 Plot of recovery factor and cumulative oil production total against Time for high salinity waterflooding (30000ppm)







Figure 26 Plot of recovery factor and cumulative oil production total against Time for High salinity (40000ppm)



Figure 27 Plot of recovery factor and cumulative oil production total against time for high salinity waterflooding (40000ppm) Table 8 Result Comparison for Low and High Salinity Waterflooding

Case	Scenario	FOE	Cumulative production	Water (%)	Time to w/c
1	Natural depletion(0-12 years)	16.5%	37.8MMstb/day	60	1
2	waterflooding (fresh water) (0-43 years)	42%	92.8 MM stb	72	2
3	Low salinity water (500ppm) (0-46 years)	52%	115.9 MM stb	71	4
4	Low salinity water (1000ppm) (0-46 years)	52%	115.9 MM stb	71	4
5	Low salinity water (1500ppm) (0-46 years)	52%	115.9 MM stb	71	4
6	Low salinity water (2000ppm) (0-46 years)	52%	115.9 MM stb	71	4
7	Low salinity water (5000ppm) (0-46 years)	49%	110.8 MM stb	71	4
8	Low salinity water (7000ppm) (0-46 years)	49%	110.8 MM stb	71	4
9	Low salinity water (10000ppm) (0-46 years)	48%	106.6 MM stb	71.8	3
10	high salinity water (30000ppm) (0-46 years)	48%	106.6 MM stb	72	2
11	high salinity water (40000ppm) (0-46 years	46%	104.8MM stb	72.5	2

#### 3.2 Discussion of Result

In natural depletion in Figure 6 and 7, oil recovery was observed to be 16.5 %. The oil production rate was maintained for one year and 4 months before oil production rate begins to drop drastically to the end of the production life of the reservoir. It was noticed that there was a sharp reduction in pressure as production continues. Field water cut was delayed for 1 and 3 months before water started coming out from the aquifer attached to the reservoir. The drop in pressure indicates that it

is practically impossible to produce from this reservoir without an additional energy to improve oil recovery, reservoir sweep and maintain pressure. Figure 7 and 8, it was observed that field oil production rate was maintained to about 2 years before a drop in oil production rate, as water production rate was high. The drop in oil production rate continues at a point, when the drop in oil production rate reduces. Field water production was maintained at zero for 2 years before we started noticing water as production continues. Water production increased steadily up to 9 years when there is a decline in the rate of water cut. However, Oil recovery was improved to 42% from 16.5% natural depletion case. Field pressure was maintained throughout the production life of the reservoir.

From Figure 9-17, oil recovery was 52%, an additional recovery of 10% was observed as compared to waterflooding(fresh water). The field pressure was maintained throughout the production life of the reservoir. The field water cut was delayed to about 4 years that means more oil will be produced.

Figure 18-21, oil recovery decreases a bit to 49% when 5000ppm salinity was injected, while pressure was maintained all through the production period. Water cut delayed to about 3 years while the field oil production rate was maintained for 2 years before a gradual decrease in oil production rate.

Figure 22-25, oil recovery was observed to be 48% when salinity of 10,000ppm and 30,000 ppm was injected into the reservoir. Field pressure was maintained throughout the production period while field water cut delayed for 3 years.

Figure 26-27, Oil recovery reduces to 46% for 40,000 ppm salinity. Field water cut was high as oil production rate reduces drastically. This indicates that in high salinity waterflooding, early water breakthrough time might be encountered as water rate was high. The mechanisms of low salinity waterflooding play out during the injection of different salt concentration.

In table 9, it can be observed that at low salinity, oil recovery improves and salinity ratio increases from (0.01-1.00). However, high salinity of 30000ppm and 40000 ppm (0.80-1.00) is almost equivalent to formation water which is 1. From the research study, residual oil saturation reduces from 0.82 to 0.44 at high salinity of 30,000ppm and 40,000ppm. The increase in salinity ratio and decrease in residual oil saturation contributes to improve oil production in all cases of low and high salinity. In table 9 and 10, it can be noticed that water cut reduces at a point increases at high salinity. This means that oil production can be improved at reduced residual oil saturation and reduced ratio of injective salinity. Also, in Figure 25, it can be observed that oil recovery improves at low salinity than high salinity.

Table 9 Residual Oil Saturation (Sorw), Salinity and Salinity Ratio

Residual oil saturation	Salinity(ppm)	Salinity Ratio	Oil Recovery (%)
0.39	500	0.01	52
0.39	1000	0.03	52
0.39	1500	0.04	52
0.39	2000	0.05	52
0.42	5000	0.13	49
0.42	7000	0.18	49
0.43	10000	0.30	48
0.43	30000	0.80	48
0.44	40000	1.00	46

# **3.2.1** Comparison of Result of the LS Case and HS Case

From the simulation study conducted, oil recovery was greatly improved at different salinity. In low salinity, oil recovery was higher as compared to high salinity. This is because the mechanisms of low salinity waterflooding was allowed to play out during the injection of low salinity water. The oil on the walls of the matrix of the rock were loose as low salt was injected, oil was displaced and mobilized. Hence, high recovery was recorded



Figure 29 Plot of residual oil saturation against salinity ratio

# 4. SENSITIVITY ANALYSIS

# 4.1 Effect of Salinity on Oil Recovery

Sensitivity analysis was carried out to examine the effect of salinity on oil recovery. Figure 27 illustrates oil recovery at different low and high salinity. It can be observed that oil recovery improved at salinity of (500-2000ppm) while at high salinity of 30000 and 40000ppm, oil recovery reduced. This means that at low salinity oil recovery is improved than high salinity as shown below in Figure 30.





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# CONCLUSION

Low salinity waterflooding was evaluated using rock and fluid properties of OML 11 F-Field in the Niger Delta. Eclipse reservoir engineering software was used to perform the reservoir simulation. In the simulation cases, waterflooding, low and high salinities of 500ppm, 1000ppm, 1500ppm, 2000ppm, 5000ppm, 7000ppm, 10000ppm, 30000ppm and 40000ppm was evaluated. Plots of field oil efficiency, oil production rates, field water cut and cumulative oil production against time were generated from the simulation study.

From the simulation results conducted in this work, the following conclusions are made:

i.Low salinity waterflooding gives a positive effect to improve oil recovery in all cases of low and high salinity.

ii. Residual oil saturation was reduced by subjecting it to waterfloods containing low salt concentrations.

iii The mechanism of fine migration, ion exchange and wettability change played a significant role in the effectiveness of oil recovery in low and high salinity.

iv. The result from the study will be useful in the industry for making choices of different salinity application and their various oil recoveries in the Niger Delta.

v.The lower the ratio of injection salinity to formation salinity , the lower the remaining oil (Sor) and the more the oil recovery increases.

vi. The optimal salinity is determined based on the economics of water treatment.

#### REFERENCES

Abdalla, A., Sun, R. Y., Tang, G. Y., Huang, A. X., & Wan, M. J. (2017, April 4). Low salinity as new technique of enhanced oil recovery. International Journal of Chemical Engineering and Application, 8(2).

- Han, D. K., Yang, C. Z., Zhang, Z. Q., Lou, Z. H., & Chang, Y. I. (1999). Recent development of enhanced oil recovery in China. *Journal of Petroleum Science Engineering*, 22, 181–189.
- Jerauld, G. R., Lin, C. Y., Webb, K. J., & Seccombe, J. C. ( 2008). *Modeling low-salinity waterflooding*. Paper SPE 102239 presented at Conference and Exhibition, San Antonio, Texas, 24–27 September.
- Morrow, N., & Buckley, J. (2011). *Improved oil recovery by low-salinity waterflooding*. Paper SPE 129421.
- Lager, A., Webb, K. J., Black, C. J. J., Singleton, M., & Sorbie, K. S. (2006). Low salinity oil recovery, an experimental investigation, paper society of core analysis (SCA) 2006-36 presented at the International Symposium of the Society of Core Analysis, Trondheim, Norway, September 2006.
- Lager, A., Webb, K. J., Collins, R., & Richmond, D. M. (2008). Enhanced oil recovery: Evidence of enhanced oil recovery at the reservoir scale. Paper SPE 113976 presented at the 2008 SPE/DOE Improved Oil Recovery Symposium held in Tulsa, Oklahoma, USA
- Levitt, D. B., & Pope, G. A. (2008). Selection and screening of polymers for enhanced- oil recovery. Paper SPE 113845 presented at the SPE Improved Oil Recovery Symposium held in Tulsa, Oklahoma, U.S.A., 19-23 April.
- Ligthelm, D. I., Gronsveld, J., Hoffman, I. P., Brusse, NJ., Marcelis, F., & Van Der Linde, H. (2009). Waterflooding strategy by manipulation of injection brine composition. Paper SPE 119835.
- Robertson, E. P. (2003). Improved waterflooding through injection-brinemodification, Idaho national engineering and environmental laboratory. Technical Report IN EEL/EXT -02-01591, Idaho Falls, Idaho, January 2003.

PPENDIX			Continued		
ractional Flov	v Table for Waterf	flooding	Sw	kro	krw
Sw	Wate	erflooding	0.22	0.698682	0.000857
511		fw	0.24	0.650595	0.001929
0.18		0	0.26	0.604222	0.003429
0.2	0.00	02826456	0.28	0.559563	0.005357
0.22		12345679	0.3	0.516619	0.007715
0.24		30221625	0.32	0.475389	0.0105
0.26		58139535	0.34	0.435874	0.013715
0.28		97580016	0.36	0.398072	0.017358
0.3		49501661	0.38	0.361986	0.021429
0.32		13973799	0.4	0.327613	0.025929
0.34		39855072	0.42	0.294955	0.030858
0.36	0.37	74653099	0.44	0.264011	0.036215
0.38		64684015	0.46	0.234781	0.042001
0.4		5555556	0.48	0.207266	0.048216
0.42	0.64	42857143	0.5	0.181465	0.054859
0.44	0.72	22840034	0.52	0.157379	0.061931
0.46	0.79	92880259	0.54	0.135007	0.069431
0.48	0.85	51627555	0.56	0.114349	0.07736
0.5	0.89	98876404	0.58	0.095405	0.085717
0.52	0.93	35275081	0.6	0.078176	0.094503
0.54	0.96	51995249	0.62	0.062661	0.103718
0.56	0.9	8044541	0.64	0.048861	0.113361
0.58	0.99	92063492	0.66	0.036775	0.123433
0.6	0.99	98189226	0.68	0.026403	0.133933
0.62		1	0.7	0.017746	0.144862
			0.72	0.010802	0.156219
elative Perme	eability of Oil and	Water	0.74	0.005574	0.168006
Sw	kro	krw	0.76	0.002059	0.18022
0.18	0.8	0	0.78	0.000259	0.192864
0.2	0.748484	0.000214	0.8	0.000174	0.205935

To be continued